

MODULE-4

EC 368-ROBOTICS

Overview

Module 5

Forward Kinematics :- Link Coordinates, D-H Repn., Appln of DH convention to different serial kinematic arrangements fitted with spherical wrist.

Inverse Kinematics :- General properties of solutions, kinematic Decoupling, Inverse kinematic solutions for all basic types of three link robotic arms fitted with a spherical wrist.

No: of hours assigned : 9 hrs.

No: of hours taken : 7 hrs

Forward Kinematics : Determine the position and orientation of the end-effector given values for the joint variables of the robot.

Robot manipulator - set of links connected together by joints.

Revolute, Pneumatic | Ball & Socket joint | Spherical Wrist

[single DOF] [2 DOF] [3 DOF]

angle of rotation displacement

Links - 0 to n

Joints - 1 to n

Joint variable denoted by q_i
 $q_i = \begin{cases} \alpha_i & \text{if joint } i \text{ is revolute} \\ \delta_i & \text{" " pneumatic.} \end{cases}$

$$H = \begin{bmatrix} R_n^\circ & a_n^\circ \\ 0 & 1 \end{bmatrix}$$

$$A_i = \begin{bmatrix} R_i^{i-1} & O_i^{i-1} \\ 0 & 1 \end{bmatrix}$$

Homogeneous Transformation -

D-H convention

► $\text{Rot}(z, \theta_i)^* \text{Trans}(z, d_i)^* \text{Trans}(x, a_i)^* \text{Rot}(x, \alpha_i)$

$C\theta_i$	$-S\theta_i$	0	0
$S\theta_i$	$C\theta_i$	0	0
0	0	1	d_i
0	0	0	1

1	0	0	a_i
0	$C\alpha_i$	$-S\alpha_i$	0
0	$S\alpha_i$	$C\alpha_i$	0
0	0	0	1

X

$C\theta_i$	$-S\theta_i C\alpha_i$	$S\alpha_i S\theta_i$	$a_i C\theta_i$
$S\theta_i$	$C\alpha_i C\theta_i$	$-S\alpha_i C\theta_i$	$a_i S\theta_i$
0	$S\alpha_i$	$C\alpha_i$	d_i
0	0	0	1



Denavit - Hartenberg Convention

Each homogeneous transformation, A_i is represented as a pdt of 4 basic transformations.

$$A_i = \text{Rot}_{x, \theta_i} \text{Trans}_{x, d_i} \text{Trans}_{x, \alpha_i} \text{Rot}_{x, \alpha_i}$$

$$= \begin{bmatrix} C\theta_i & -S\theta_i & 0 & 0 \\ S\theta_i & C\theta_i & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\alpha_i & S\alpha_i & 0 \\ 0 & S\alpha_i & C\alpha_i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} C\theta_i & -S\theta_i C\alpha_i & S\alpha_i S\theta_i & a_i C\theta_i \\ S\theta_i & C\theta_i C\alpha_i & -C\theta_i S\alpha_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$\theta_i, a_i, d_i, \alpha_i$ - parameters associated with link i and joint i

θ_i - joint angle [revolute]

a_i - link length (constant)

d_i - link offset [for prismatic]

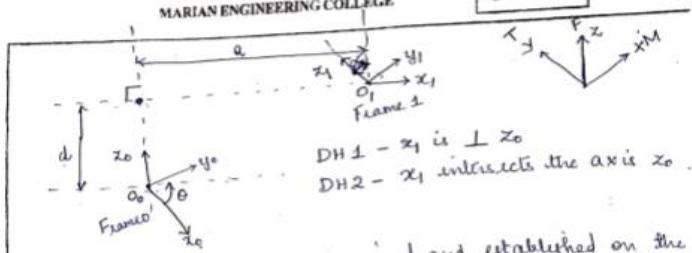
α_i - link twist.

Homogeneous Transformation Matrix - six numbers

[3 Euler angles + 3 nos to specify the 4th column of the matrix]

6 parameters are cut down to four (4).

Continued....



Every co-ordinate frame is determined and established on the basis of 3 rules :-

- ① x_i axis lies along the axis of motion of the i^{th} joint.
[x_0 lies along 1st joint]
- ② x_i axis is normal to the x_{i-1} axis and pointing away from it.
[x_i is normal to x_0]
- ③ The y_i axis completes the right handed coordinate system as required.

Location of frame 0 coordinate - in base.

Last frame coordinate (n^{th} frame) - in hand.
as long as x_n normal to x_{n-1}

Four parameters to describe revolute / prismatic

* α_i - joint angle from x_{i-1} axis to the x_i axis abt x_{i-1} axis (st hand rule).

[$x_0 \rightarrow x_i$ abt x_0]

* d_i - distance from the origin of $(i-1)^{\text{th}}$ coordinate frame to the intersection of the x_{i-1} axis with x_i axis along x_{i-1} axis.

Continued....

- * a_i - offset distance from the intersection of the x_{i-1} axis with the x_i axis to the origin of the i^{th} frame along x_i axis (shortest distance b/w the x_{i-1} axis & x_i axis)
- * α_i - offset angle from the x_{i-1} axis to the x_i axis abt the x_i axis (st hand rule) [z_0 to z_1 , abt x_1]

Assigning coordinate frames:-

Establish x axes for the links.

- * Design x_i to be the axis of actuation for joint $i+1$

$[x_0]$

2 cases:-

- (i) if joint $i+1$ is revolute, x_i axis of revolution of joint $i+1$
- (ii) " prismatic, " translation "

when joint i is activated abt axis x_{i-1} , link i and frame $Ox_0x_1x_i$ results in a motion.

Establish base frame.

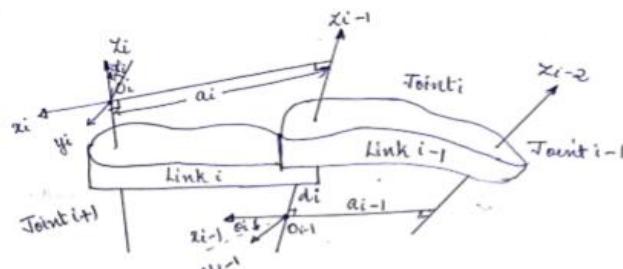
Choose x_0, y_0 in a convenient manner so long as the resulting frame is st handed. This is frame O .

After establishing frame O , then define frame i using $i-1$

To set up frame i :-

- (i) x_{i-1}, x_i are not coplanar
- (ii) x_{i-1}, x_i intersect } coplanar
- (iii) x_{i-1}, x_i are parallel }

D-H frame Assignment



D-H Frame Assignment

(i) x_{i-1} and x_i are not coplanar $[d_{i-1}^*, \alpha_i^*]$
 x_{i-1} to $x_i \rightarrow \alpha_i$ as not coplanar (to make it coplanar)
 $\rightarrow a_i$ (shortest line segment from x_{i-1} to x_i)
 \perp to x_{i-1} and x_i

The line segment is a_i and the point where it intersects x_i is the origin O_i . Satisfies $x_i \perp z_0$ (DH1)
 x_i intersects z_0 (DH2)

So, $A_i = \text{Rot}_{x, \alpha_i} \text{Trans}_{x, d_i} \text{Trans}_{x, a_i} \text{Rot}_{x, \alpha_i}$

(ii) x_{i-1} is \parallel to x_i $[d_i = 0, \alpha_i^*]$
 So many normals are present. Free to choose origin
 O_i anywhere along x_i (for simplifying)

Normal method to choose O_i is to choose the normal
 that passes thru O_{i-1} as x_i axis. O_i is then the pt.
 at which this normal intersects x_i . $d_i = 0$.

\therefore the x_{i-1} and x_i are \parallel , $\alpha_i = 0$.

(iii) x_{i-1} intersects x_i $[a_i = 0]$

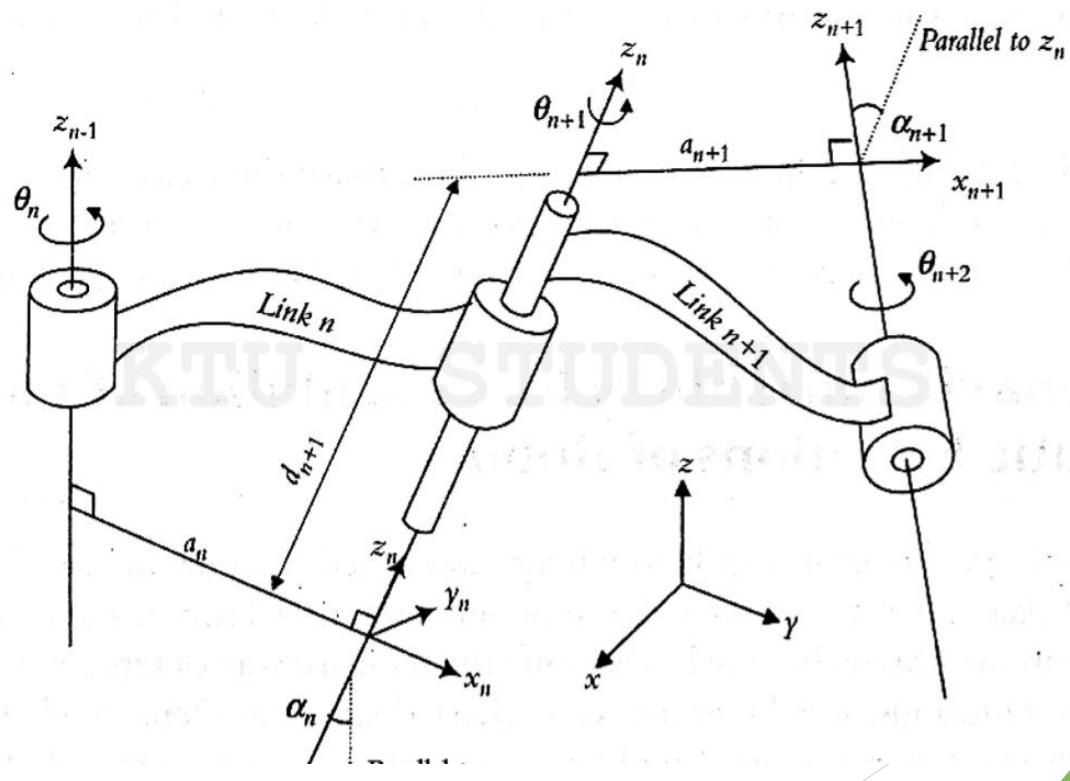
x_i is normal to the plane formed by x_i and x_{i-1}

LINK COORDINATES

Joint n

Joint n+1

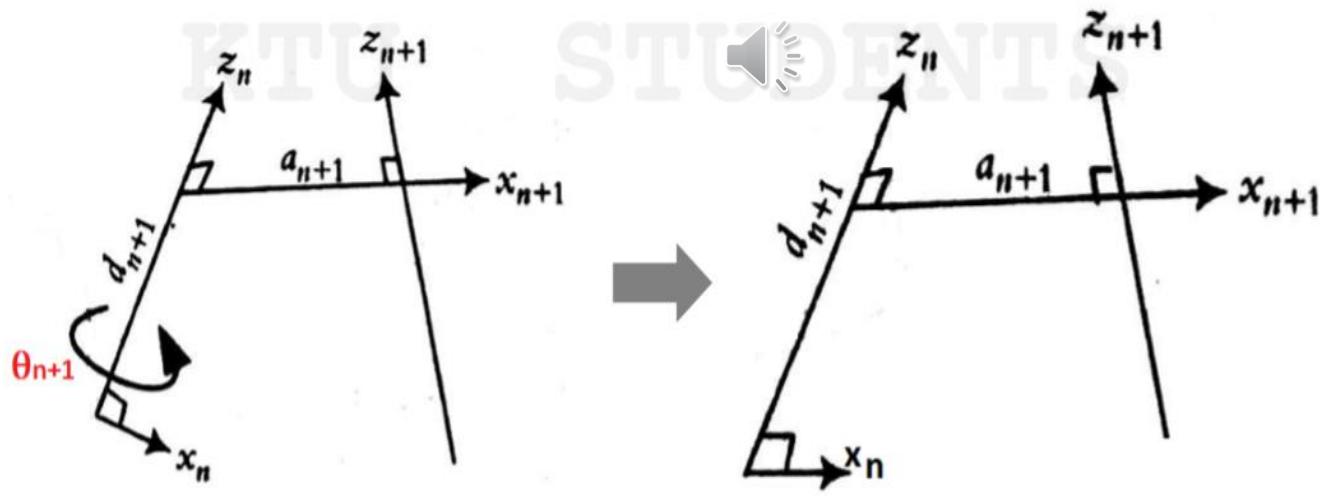
Joint n+2



To find DH parameter (θ_{n+1} -joint angle)

1. Rotate the joint at angle θ_{n+1} about the z_n -axis.

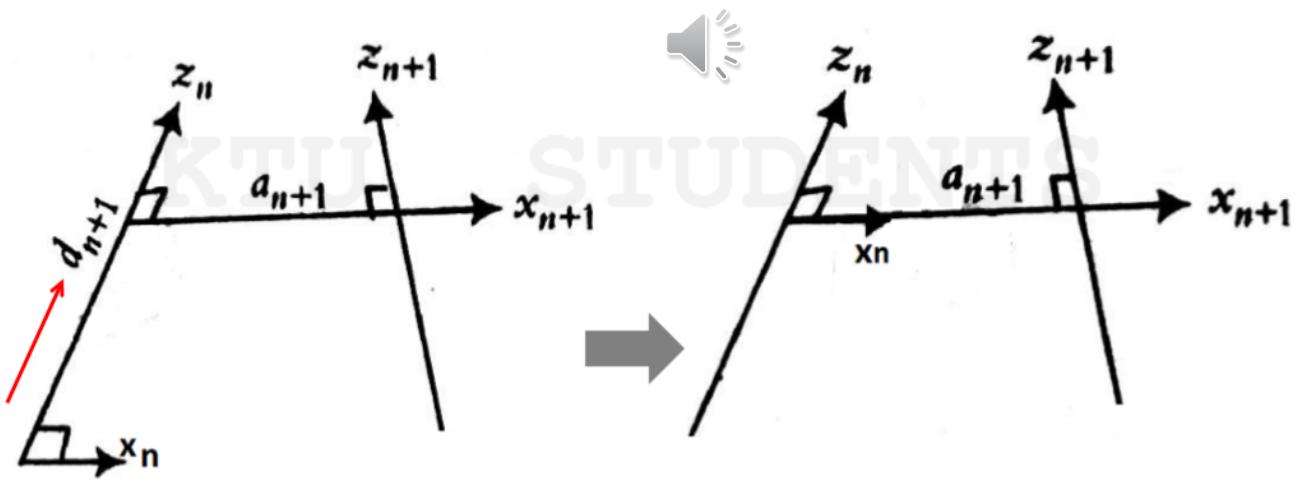
This will make x_n and x_{n+1} parallel to each other



To find DH parameter (di-link offset)

2. Translate along z_n -axis a distance d_{n+1} .

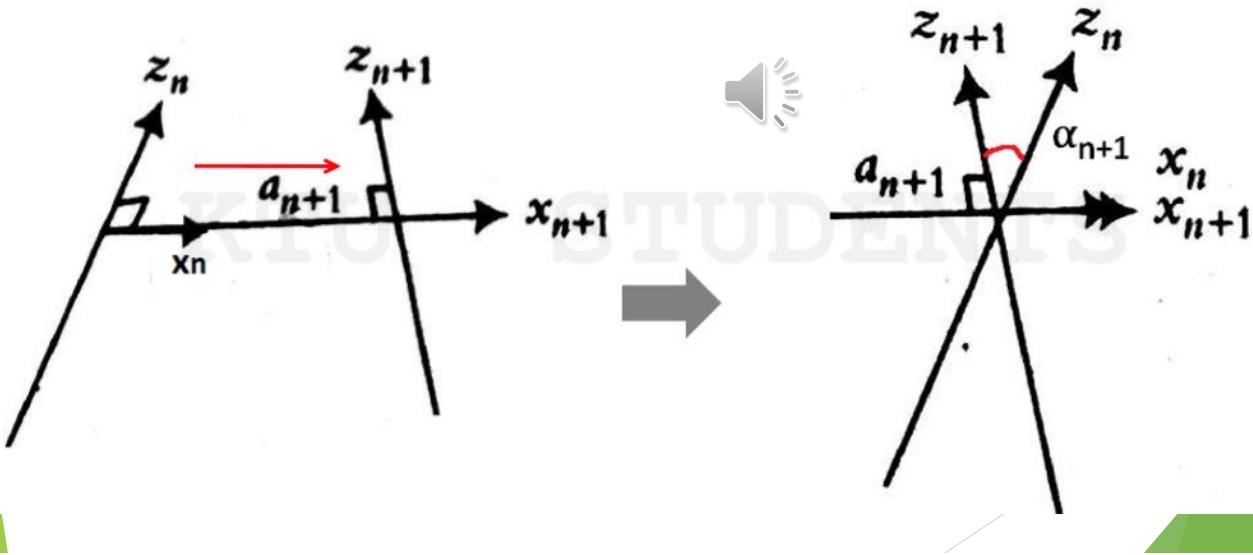
This will make x_n and x_{n+1} colinear.



To find DH parameter (ai-link length)

3. Translate along x_n - axis a distance a_{n+1} .

This will bring the origins of x_n and x_{n+1} . That is the two origins will be the same.

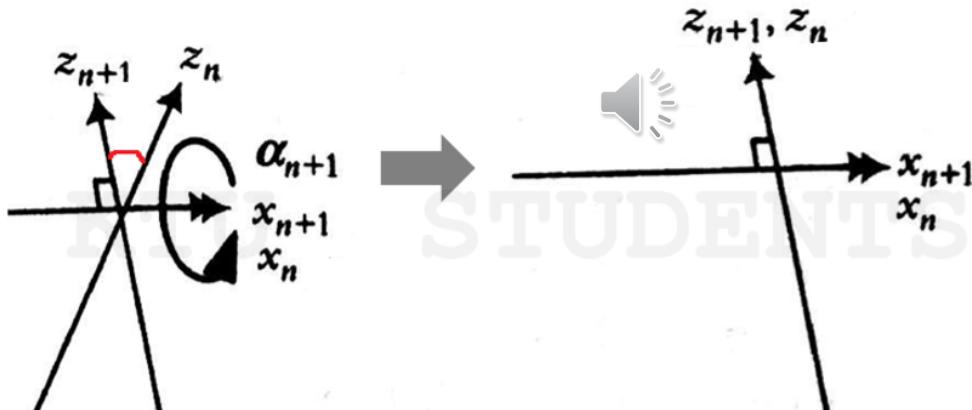


To find DH parameter (α -link twist)

4. Rotate the z_n -axis at angle α_{n+1} about the x_{n+1} -axis.

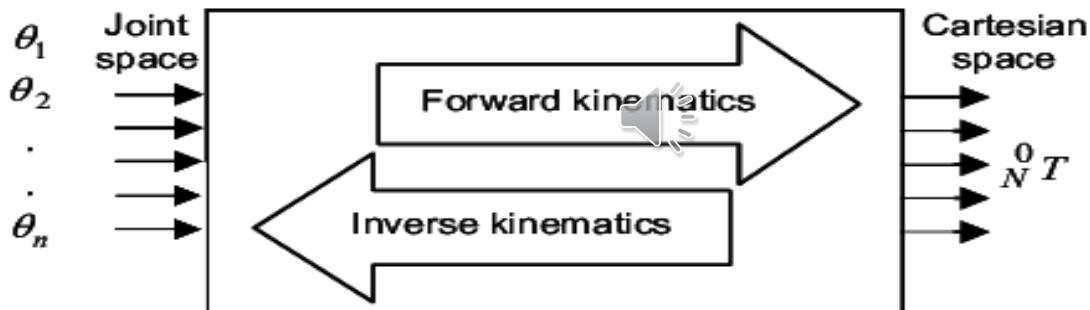
This will make z_n to align with z_{n+1} axis.

So the frame n and $n+1$ will be exactly same and we have transformed from one frame to the next.

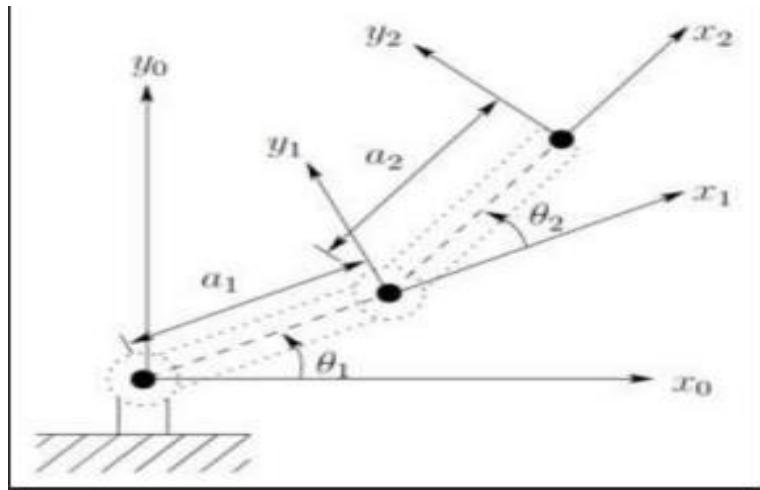


Angle is taken positive when rotation is made counter clockwise.

What is Forward Kinematics and Inverse Kinematics?



2 link Planar Manipulator(RR)



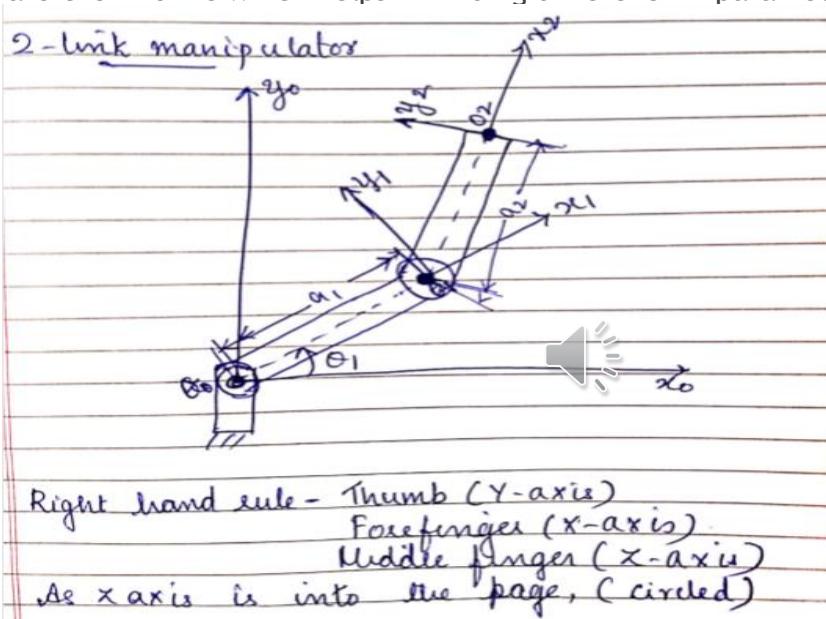
Link	a_i	α_i	d_i	θ_i
1	a_1	0	0	θ_1^*
2	a_2	0	0	θ_2^*

* variable

- ▶ Explained earlier

1. How to find DH parameter table for a 2 link planar manipulator

- These are the 4 forms which helps in finding different DH parameters



Link	θ_i	d_i	a_i	α_i
1	θ_1^*	0	a_1	0
2	θ_2^*	0	a_2	0

To find Homogenous Transformation Matrix

- Transformation matrix is represented as $A_i = \text{Rot}(z, \theta_i) * \text{Trans}(z, d_i) * \text{Trans}(x, a_i) * \text{Rot}(x, \alpha_i)$

$$\text{Rot}(x, \alpha_i) = \begin{bmatrix} C\alpha_i & -S\alpha_i & 0 & 0 \\ S\alpha_i & C\alpha_i & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\text{Trans}(x, d_i) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\text{Trans}(x, a_i) = \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\text{Rot}(x, \alpha_i) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\alpha_i & -S\alpha_i & 0 \\ 0 & S\alpha_i & C\alpha_i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

By matrix multiplication

$$A_i = \begin{bmatrix} C\alpha_i & -S\alpha_i C\alpha_i & S\alpha_i S\alpha_i & a_i C\alpha_i \\ S\alpha_i & C\alpha_i C\alpha_i & -C\alpha_i S\alpha_i & a_i S\alpha_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

From the given For 2 link manipulator
link 1 $\rightarrow \theta_1, a_1, \alpha_1 = 0, d_1 = 0$.

$$A_1 = \begin{bmatrix} C\theta_1 & -S\theta_1 & 0 & a_1 C\theta_1 \\ S\theta_1 & C\theta_1 & 0 & a_1 S\theta_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Link 2 $\rightarrow \theta_2, a_2, \alpha_2 = 0, d_2 = 0$.

$$A_2 = \begin{bmatrix} C\theta_2 & -S\theta_2 & 0 & a_2 C\theta_2 \\ S\theta_2 & C\theta_2 & 0 & a_2 S\theta_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2^0 = A_1 \cdot A_2 = \cos(\theta_1 + \theta_2) \quad \sin(\theta_1 + \theta_2) \quad a_1 \cos(\theta_1 + \theta_2) \quad d_2$$

(Homogeneous Transformation Matrix)

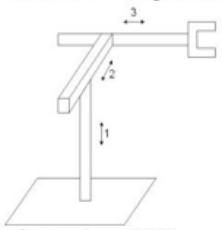
$$= \begin{bmatrix} C_{12} & -S_{12} & 0 & a_1 C_1 + a_2 C_{12} \\ S_{12} & C_{12} & 0 & a_1 S_1 + a_2 S_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$C_{12} = \cos(\theta_1 + \theta_2)$$

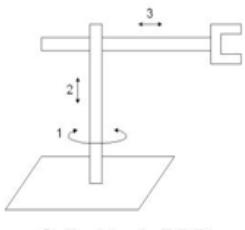
$$S_{12} = \sin(\theta_1 + \theta_2)$$

Manipulators

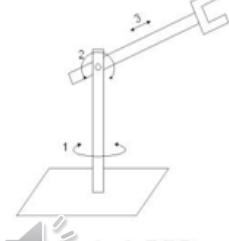
- Robot Configuration:



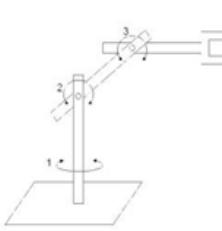
Cartesian: PPP



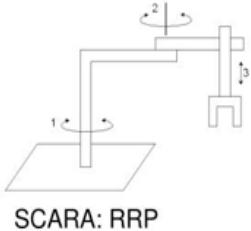
Cylindrical: RPP



Spherical: RRP



Articulated: RRR



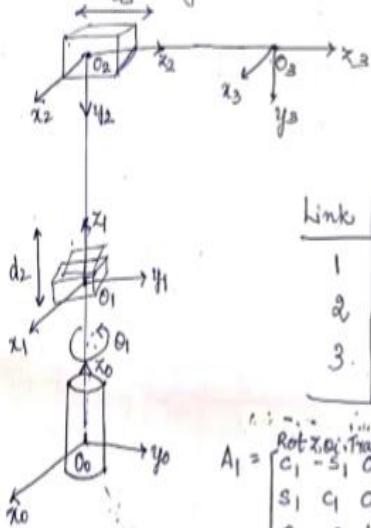
SCARA: RRP
(Selective Compliance Assembly Robot Arm)

Hand coordinate:

n: normal vector; **s**: sliding vector;
a: approach vector, normal to the
tool mounting plate

2. 3 link cylindrical robot(RPP)

① Three link cylindrical robot (RPP)



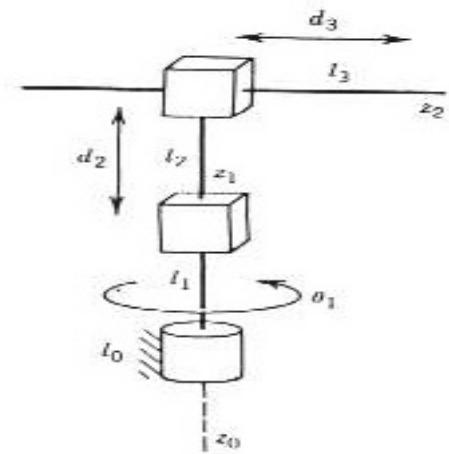
$x_i \text{ unlabeled } x_{i-1}, \theta_i = 0$
 $x_i \parallel x_{i-1}, \alpha_i = 0$
 $O_i = O_{i-1}; d_i$

Link	Joint angle	Link offset	Link twist	Link frame
1	θ_1^*	d_1	0	0
2	0	d_2^*	0	-90°
3	0	d_3	0	0



$$A_1 = \begin{bmatrix} \text{Rot}_z, \theta_1, \text{Trans}_x, d_1 \\ C_1 & -S_1 & 0 & 0 \\ S_1 & C_1 & 0 & 0 \\ 0 & 0 & 1 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad A_2 = \begin{bmatrix} \text{Trans}_z, d_2, \text{Rot}_x, 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

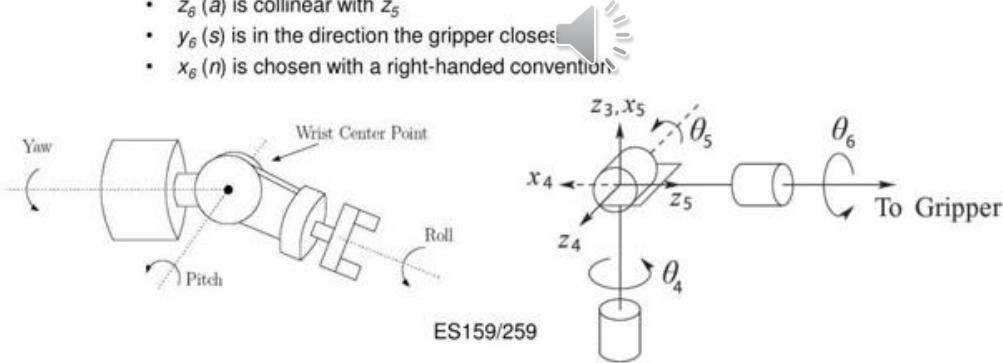
$$A_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \text{Trans}_x, d_3$$



$$T_3^0 = \begin{bmatrix} C_1 & 0 & -S_1 & -S_1 d_3 \\ S_1 & 0 & C_1 & C_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Example 3: spherical wrist

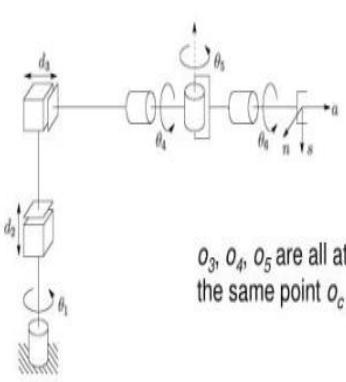
- 3DOF: need to assign four coordinate frames
 - yaw, pitch, roll ($\theta_4, \theta_5, \theta_6$) all intersecting at one point o (wrist center)
 - 1. Choose z_3 axis (axis of rotation for joint 4)
 - 2. Choose z_4 axis (axis of rotation for joint 5)
 - 3. Choose z_5 axis (axis of rotation for joint 6)
 - 4. Choose tool frame:
 - z_6 (a) is collinear with z_5
 - y_6 (s) is in the direction the gripper closes
 - x_6 (n) is chosen with a right-handed convention



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Example 4: cylindrical robot with spherical wrist

- 6DOF: need to assign seven coordinate frames
 - But we already did this for the previous two examples, so we can fill in the table of DH parameters:



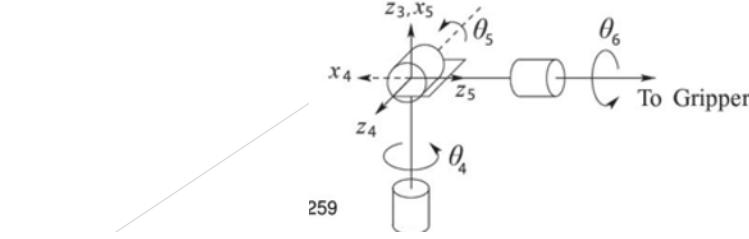
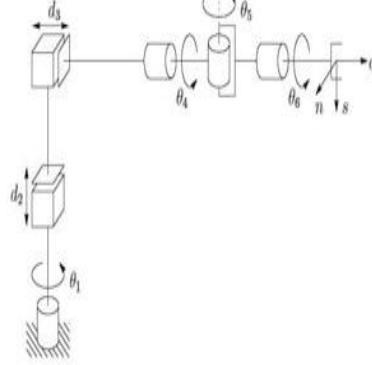
o_3, o_4, o_5 are all at the same point o_c

link	a_i	α_i	d_i	θ_i
1	0	0	d_1	θ_1
2	0	-90	d_2	0
3	0	0	d_3	0
4	0	-90	0	θ_4
5	0	90	0	θ_5
6	0	0	d_6	θ_6

- Note that z_3 (axis for joint 4) is collinear with z_2 (axis for joint 3), thus we can make the following combination:

$$T_6^0 = T_3^0 T_6^3 = \begin{bmatrix} r_{11} & r_{12} & r_{13} & d_x \\ r_{21} & r_{22} & r_{23} & d_y \\ r_{31} & r_{32} & r_{33} & d_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

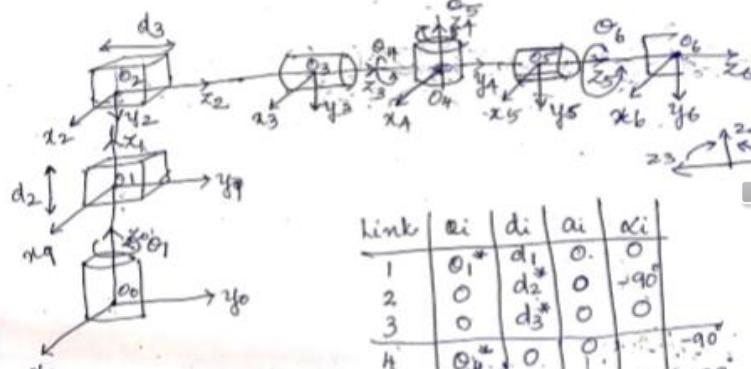
$$\left. \begin{array}{l} r_{11} = C_1 C_4 C_5 C_6 - C_1 S_4 S_6 + S_1 S_5 C_6 \\ r_{21} = S_1 C_4 C_5 C_6 - S_1 S_4 S_6 - C_1 S_5 C_6 \\ r_{31} = -S_1 C_5 C_6 - C_4 S_6 \\ r_{12} = -C_1 C_4 C_5 S_6 - C_1 S_4 C_6 - S_1 S_5 C_6 \\ r_{22} = -S_1 C_4 C_5 S_6 - S_1 S_4 S_6 + C_1 S_5 C_6 \\ r_{32} = S_4 C_5 C_6 - C_4 C_6 \\ r_{13} = C_1 C_4 S_5 - S_1 C_5 \\ r_{23} = S_1 C_4 S_5 + C_1 C_5 \\ r_{33} = -S_4 S_5 \\ d_x = C_1 C_4 S_5 d_6 - S_1 C_5 d_6 - S_1 d_3 \\ d_y = S_1 C_4 S_5 d_6 + C_1 C_5 d_6 + C_1 d_3 \\ d_z = -S_4 S_5 d_6 + d_1 + d_2 \end{array} \right\}$$



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3.Cylindrical manipulator with spherical wrist (RPP+spherical wrist(3 DOF)=6 DOF)

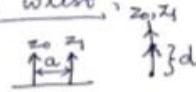
③ Cylindrical manipulator with spherical wrist



Link	α_i	d_i	a_i	κ_i
1	O_1^*	d_1^*	0.	0
2	0	d_2^*	0	-90°
3	0	d_3^*	0	0
4	O_4^*	0.	0	-90°
5	O_5^*	0	0	+90°
6	O_6^*	d_6	0	0.

$$A_4 = \begin{bmatrix} \cos \theta_4 & 0 & -\sin \theta_4 & 0 \\ \sin \theta_4 & 0 & \cos \theta_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_5 = \begin{bmatrix} \cos \theta_5 & 0 & +\sin \theta_5 & 0 \\ \sin \theta_5 & 0 & \cos \theta_5 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



$$A_1 \cdot A_2 \cdot A_3 = T_3^0$$

$$T_6^3 = A_4 \cdot A_5 \cdot A_6$$

$$A_4 = \begin{bmatrix} c_4 & 0 & -s_4 & 0 \\ s_4 & 0 & c_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad A_5 = \begin{bmatrix} c_5 & 0 & s_5 & 0 \\ s_5 & 0 & -c_5 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_6 = \begin{bmatrix} c_6 & -s_6 & 0 & 0 \\ s_6 & c_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_6^3 = \begin{bmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_4 c_5 s_6 - s_4 c_6 & c_4 s_5 & c_4 s_5 d_6 \\ s_4 c_5 c_6 + c_4 s_6 & -s_4 c_5 s_6 + c_4 c_6 & s_4 s_5 & s_4 s_5 d_6 \\ -s_5 c_6 & s_5 s_6 & c_5 & c_5 - d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_6^0 = T_3^0 \cdot T_6^3$$

$$= \begin{bmatrix} g_{11} & g_{12} & g_{13} & dx \\ g_{21} & g_{22} & g_{23} & dy \\ g_{31} & g_{32} & g_{33} & dz \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$g_{33} = -s_4 s_5 \\ dx = c_4 c_5 s_6 d_6 - s_4 c_5 d_6 - s_4 d_3$$

$$\begin{aligned} g_{11} &= c_4 c_5 c_6 - c_4 s_5 s_6 + s_4 s_5 c_6 \\ g_{21} &= s_4 c_4 c_5 c_6 - s_4 s_4 s_6 - c_4 c_5 - c_6 \\ g_{31} &= -s_4 c_5 c_6 - c_4 s_6 \\ g_{12} &= -c_4 c_4 c_5 s_6 - c_4 s_4 c_6 - s_4 s_5 c_6 \\ g_{22} &= -s_4 c_4 c_5 s_6 - s_4 s_4 s_6 + c_4 s_5 c_6 \\ g_{32} &= s_4 c_5 c_6 - c_4 c_6 \\ g_{13} &= c_4 c_5 s_6 d_6 - s_4 c_5 d_6 - s_4 d_3 \end{aligned}$$

should this
be d_1 ?

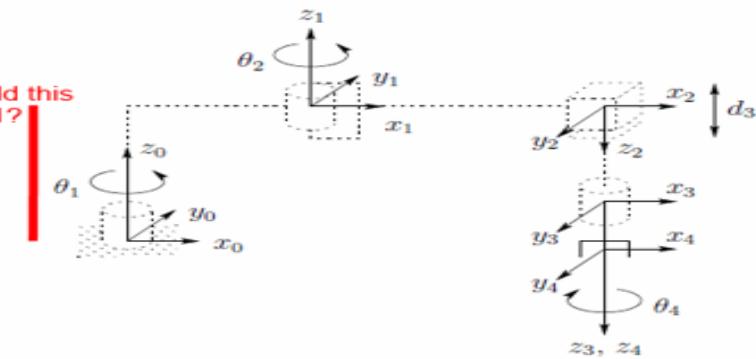


Fig. 3.11 DH coordinate frame assignment for the SCARA manipulator

Table 3.5 Joint parameters for SCARA

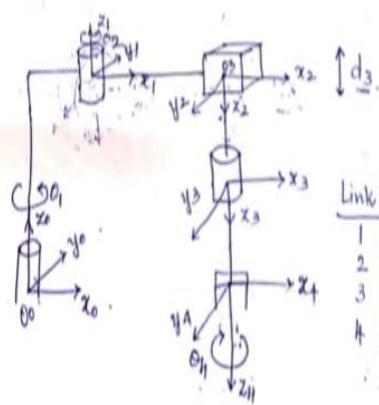
Link	a_i	α_i	d_i	θ_i
1	a_1	0	0	θ^*
2	a_2	180	0	θ^*
3	0	0	d^*	0
4	0	0	d_4	θ^*

* joint variable

Why not d_1 ?

4. SCARA Manipulator (RRP+1 DOF=4 DOF)

(1) SCARA Manipulator (RRP+1 DOF for wrist) Jointing



Link	θ_i	d_i	a_i	α_i
1	θ_1^*	0	a_1	0
2	θ_2^*	0	a_2	180°
3	0	d_3	0	0
4	θ_4^*	d_4	0	0

link	θ_i	d_i	a_i	α_i
1	θ_1^*	0	a_1	0
2	θ_2^*	0	a_2	180°
3	0	d_3	0	0
4	θ_4^*	d_4	0	0

$$A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1 c_1 \\ s_1 & c_1 & 0 & a_1 s_1 \\ 0 & 0 & 1 & b \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} c_2 & s_2 & 0 & a_2 c_2 \\ s_2 & -c_2 & 0 & a_2 s_2 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_4 = \begin{bmatrix} c_4 & -s_4 & 0 & 0 \\ s_4 & c_4 & 0 & 0 \\ 0 & 0 & 1 & d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

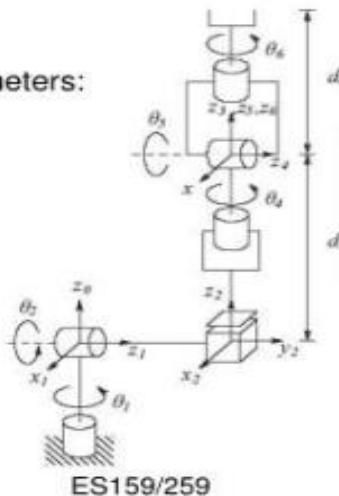
$$T_4^0 = A_1 \cdot A_2 \cdot A_3 \cdot A_4$$

$$= \begin{bmatrix} c_{12}c_4 + s_{12}s_4 & -c_{12}s_4 + s_{12}c_4 & 0 & a_1c_1 + a_2c_2 \\ s_{12}c_4 - c_{12}s_4 & -s_{12}s_4 - c_{12}c_4 & 0 & a_1s_1 + a_2s_2 \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Example 5: the Stanford manipulator

- 6DOF: need to assign seven coordinate frames:
 1. Choose z_0 axis (axis of rotation for joint 1, base frame)
 2. Choose z_1-z_5 axes (axes of rotation/translation for joints 2-6)
 3. Choose x_i axes
 4. Choose tool frame
 5. Fill in table of DH parameters:

link	a_i	α_i	d_i	θ_i
1	0	-90	0	θ_1
2	0	90	d_2	θ_2
3	0	0	d_3	0
4	0	-90	0	θ_4
5	0	90	0	θ_5
6	0	0	d_6	θ_6



*Suggested insertion:
photo of the Stanford
manipulator*