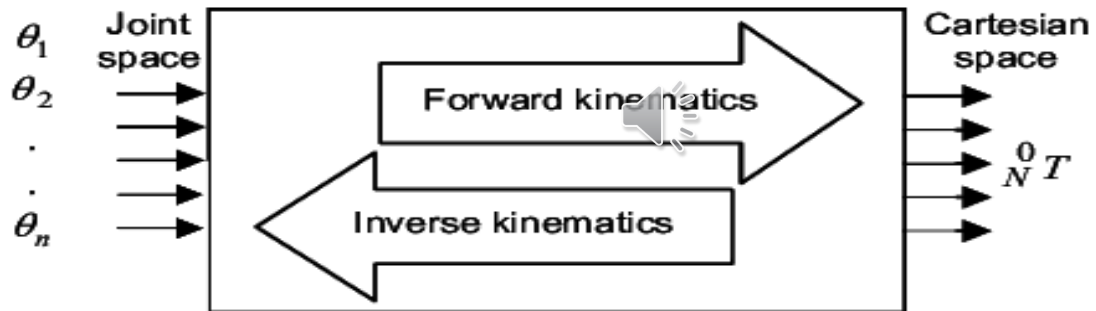


# MODULE-4-INVERSE KINEMATICS

EC 368-ROBOTICS

# What is Forward Kinematics and Inverse Kinematics?



# Problem Formulation

- Forward Kinematics

- End effector position as a function of  $q$
- We solve for  $H_n^0(q)$ .

- Inverse Kinematics

- Given  $H = T_n^0(q_1, \dots, q_n) = A_1(q_1) \dots A_n(q_n)$
- Find all joint variables  $q_1, \dots, q_n$ 
  - Can rewrite as 12 equations in  $n$  unknowns as  $T_{ij}(q_1, \dots, q_n) = h_{ij}$
  - Why not 16 equations?

- ▶ Last row is always considered as  $[0 \ 0 \ 0 \ 1]$ , neglect that row then only 12 simultaneous equations are needed for solution.

# METHODS OF SOLUTION

- ▶ We have to find joint variables in terms of the end effector position and orientation which is more difficult.
- ▶ There are two ways : (1) Algebraic approach  
(2) Geometrical approach
- ▶ In Algebraic method, end effector Position parameters (x, y and z) is obtained from Homogenous Transformation matrix.
- ▶ By applying Cosine rules
- ▶ Pythagoras theorem
- ▶ Sum of angles identities
- ▶ Use atan2 (arc tangent function)



It is used in applications involving vectors in Euclidean space ,such as finding the direction from one point to another. To convert Rotation matrix representation into Euler angle.

$\text{atan2}(y,x)$ =Cartesian to polar

Gets value of y and x and assumes a complex number as  $x+iy$  and returns its phase

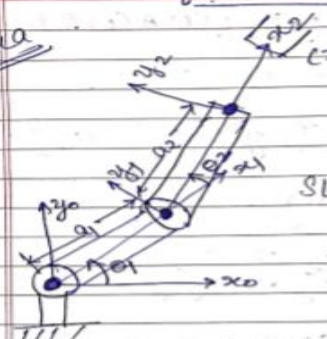
# EG: INVERSE KINEMATICS OF RR PLANAR ELBOW MANIPULATOR-ALGEBRAIC APPROACH

using algebra

To find Inverse Kinematics

From Homogeneous Transformation matrix

Step 1: Take out dx & dy values alone.


$$T_2 = \begin{bmatrix} c_{12} & -s_{12} & 0 & a_1 c_1 + a_2 c_{12} \\ s_{12} & c_{12} & 0 & a_1 s_1 + a_2 s_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{matrix} \rightarrow x \\ \rightarrow y \\ \\ \end{matrix}$$
$$c_{12} = \cos(\theta_1 + \theta_2)$$
$$s_{12} = \sin(\theta_1 + \theta_2)$$
$$x = a_1 \cos \theta_1 + a_2 \cos(\theta_1 + \theta_2)$$
$$y = a_1 \sin \theta_1 + a_2 \sin(\theta_1 + \theta_2)$$

# Continued...

$$\cos(A+B) = \cos A \cos B - \sin A \sin B$$

$$\sin(A+B) = \sin A \cos B + \cos A \sin B$$

Step 2: Squaring and adding.

$$\Rightarrow \begin{aligned} x^2 + y^2 &= \left\{ \begin{aligned} a_1^2 \cos^2 \theta_1 + a_2^2 \cos^2(\theta_1 + \theta_2) \\ + 2a_1 a_2 \cos \theta_1 \cos(\theta_1 + \theta_2) \end{aligned} \right. \\ &+ \left\{ \begin{aligned} a_1^2 \sin^2 \theta_1 + a_2^2 \sin^2(\theta_1 + \theta_2) \\ + 2a_1 a_2 \sin \theta_1 \sin(\theta_1 + \theta_2) \end{aligned} \right. \end{aligned}$$

$$\text{Let } \theta_1 = A, \theta_1 + \theta_2 = B.$$

$$\left[ \begin{aligned} \cos \theta_1 \cdot \cos(\theta_1 + \theta_2) + \sin \theta_1 \sin(\theta_1 + \theta_2) \\ = \cos A \cos B + \sin A \sin B \\ = \cos(A-B) \end{aligned} \right]$$

∴  $\cos^2 \theta + \sin^2 \theta = 1$

$$\Rightarrow a_1^2 + a_2^2 + 2a_1 a_2 \cos[\theta_1 - \theta_1 - \theta_2]$$

$$\vec{x} + \vec{y} \Rightarrow a_1^2 + a_2^2 + 2a_1 a_2 \cos \theta_2 \rightarrow \textcircled{1}$$

$$\cos \theta_2 = \frac{x^2 + y^2 - a_1^2 - a_2^2}{2a_1 a_2}$$

$$\theta_2 = \cos^{-1} \left[ \frac{x^2 + y^2 - a_1^2 - a_2^2}{2a_1 a_2} \right] \Rightarrow \textcircled{A}$$

# Continued...

Step 3: Apply sum of angles identities of

Substitute  $\cos \theta_2 \rightarrow C_2$   
 $\sin \theta_2 \rightarrow S_2$

$$x = (a_1 + a_2 C_2) \cos \theta_1 - a_2 S_2 \sin \theta_1$$

$$y = (a_1 + a_2 C_2) \sin \theta_1 + a_2 S_2 \cos \theta_1$$

obtained from:

$$x = a_1 c_1 + a_2 (c_1 c_2 - s_1 s_2)$$

$$= (a_1 + a_2 c_2) c_1 - a_2 s_2 s_1$$

$$y = a_1 s_1 + a_2 (s_1 c_1 + c_1 s_1)$$

$$= (a_1 + a_2 c_1) s_1 + a_2 s_2 c_1$$

Consider y:

$$y = (a_1 + a_2 c_2) \sin \theta_1 + a_2 s_2 \cos \theta_1 \rightarrow \text{⑥}$$

Note:

$$a \cos \theta + b \sin \theta = c$$

$$\theta = \tan^{-1} \frac{c}{\sqrt{a^2 + b^2 - c^2}} = \tan^{-1} \left( \frac{a}{b} \right)$$

# Continued...

From (2)

$$a = a_2 s_2; \quad b = a_1 + a_2 c_2; \quad c = y$$

$$\theta_1 = \tan^{-1} \frac{y}{\sqrt{a_2^2 s_2^2 + a_1^2 + a_2^2 c_2^2 + 2a_1 a_2 c_2 - y^2}}$$

$$- \tan^{-1} \left( \frac{a_2 s_2}{a_1 + a_2 c_2} \right)$$

$$\theta_1 = \tan^{-1} \left( \frac{y}{\sqrt{a_1^2 + a_2^2 + 2a_1 a_2 c_2 - y^2}} \right) - \tan^{-1} \left( \frac{a_2 s_2}{a_1 + a_2 c_2} \right)$$

From (1)  $x^2 + y^2 = a_1^2 + a_2^2 + 2a_1 a_2 c_2$

$$\theta_1 = \tan^{-1} \left( \frac{y}{\sqrt{x^2 + y^2 - y^2}} \right) - \tan^{-1} \left( \frac{a_2 s_2}{a_1 + a_2 c_2} \right)$$

$$\theta_1 = \tan^{-1} \left( \frac{y}{x} \right) - \tan^{-1} \left( \frac{a_2 s_2}{a_1 + a_2 c_2} \right) \Rightarrow \text{(B)}$$

Joint variables of RR (2 link planar elbow)  $\theta_1$  and  $\theta_2$  is thus found out (manipulator)



## Redundant solution:

Redundant solutions are available while performing Inverse Kinematics

$$\cos \theta_2 = \frac{x^2 + y^2 - a_1^2 - a_2^2}{2a_1 a_2}$$

$$\sin \theta_2 = \pm \sqrt{1 - \cos^2 \theta_2}$$

So  $\theta_2$  cannot be confirmed as  $\cos^{-1}$

There comes the importance of  $\text{atan2}$

$$\theta_2 = \text{atan2}(\sin \theta_2, \cos \theta_2)$$

$$\boxed{\theta_2 = \text{atan2}(s_2, c_2)}$$

Condition for this solution to exist:

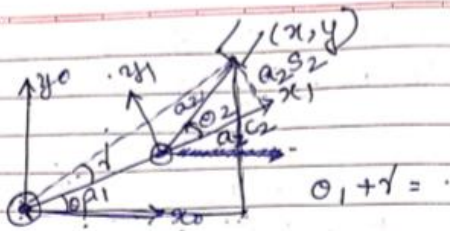
$$\text{if } -1 \leq c_2 \leq 1$$

$$-1 \leq \frac{x^2 + y^2 - a_1^2 - a_2^2}{2a_1 a_2} \leq 1$$

Rewriting

$$(a_1 - a_2)^2 \leq x^2 + y^2 \leq (a_1 + a_2)^2$$

# Continued...



$$\sin \theta_2 = \frac{\text{opp}}{a_2} ; \text{opp} = a_2 \sin \theta_2$$

$$\cos \theta_2 = \frac{\text{adj}}{a_2} ; \text{adj} = a_2 \cos \theta_2$$

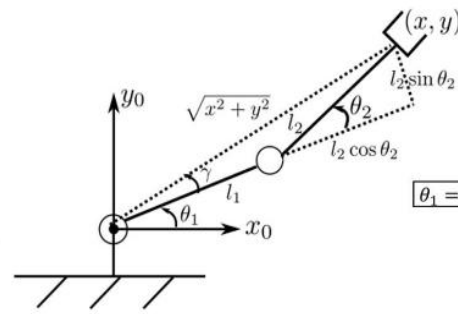
$$\tan(\theta_1 + \gamma) = \frac{y}{x}$$

$$\theta_1 + \gamma = \text{atan2}(y, x)$$

$$\gamma = \text{atan2}(a_2 \sin \theta_2, a_1 + a_2 \cos \theta_2)$$

$$\theta_1 = \text{atan2}(y, x) - \text{atan2}(a_2 \sin \theta_2, a_1 + a_2 \cos \theta_2)$$

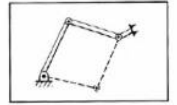
## Solve for $\theta_1$



$$\theta_1 + \gamma = \text{atan2}(y, x)$$

$$\gamma = \text{atan2}(l_2 \sin \theta_2, l_1 + l_2 \cos \theta_2)$$

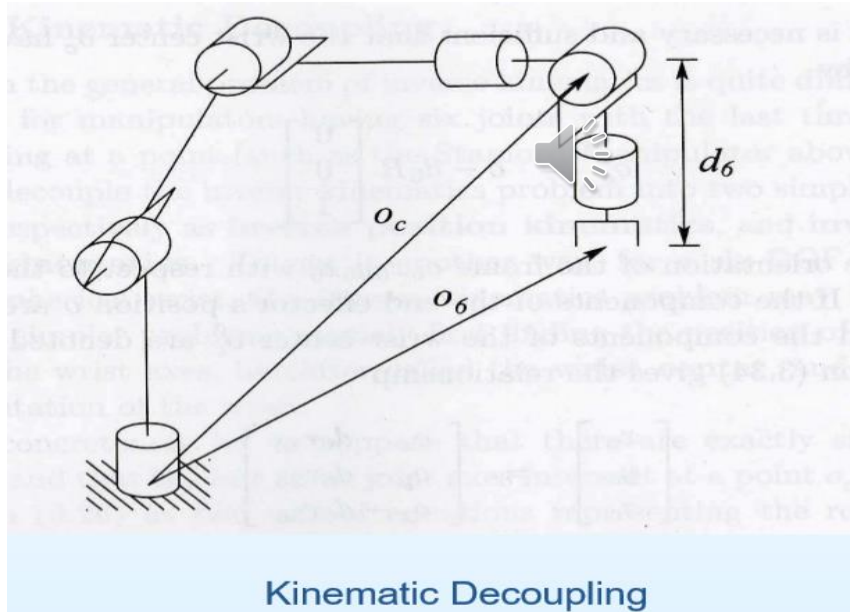
$$\theta_1 = \text{atan2}(y, x) - \text{atan2}(l_2 \sin \theta_2, l_1 + l_2 \cos \theta_2)$$

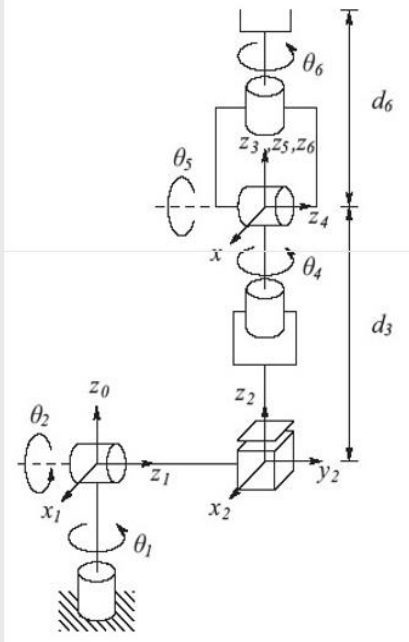


2 solutions:  
elbow up,  
elbow down

# KINEMATIC DECOUPLING

- ▶ Some complicated problems like Stanford manipulator and for manipulators with 6 DOF with last 3 joint axes intersect at a point (wrist centre), general IK is difficult So Kinematic decoupling is done.
- ▶ For that Decouple into two solutions: inverse position of wrist centre  
inverse orientation of wrist centre





link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	-90	0	$\theta_1^*$
2	0	90	$d_2$	$\theta_2^*$
3	0	0	$d_3^*$	0
4	0	-90	0	$\theta_4^*$
5	0	90	0	$\theta_5^*$
6	0	0	$d_6$	$\theta_6^*$

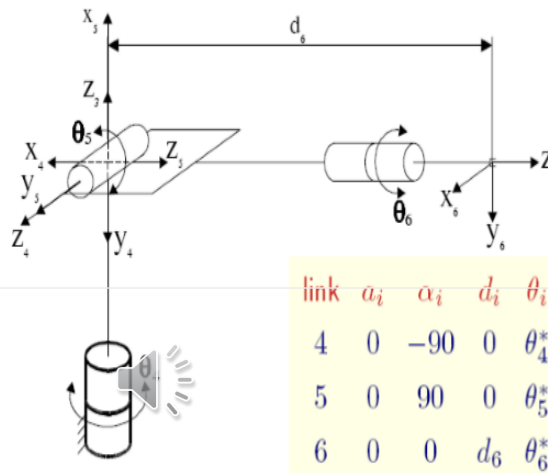
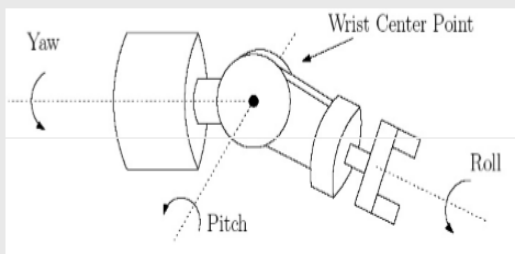
$$A_i = \begin{bmatrix} c\theta_i & -s\theta_i c\alpha_i & s\theta_i s\alpha_i & a_i c\theta_i \\ s\theta_i & c\theta_i c\alpha_i & -c\theta_i s\alpha_i & a_i s\theta_i \\ 0 & s\alpha_i & c\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- IK problem: for given  $R$  and  $o$  solve 9 rotational and 3 positional equations:

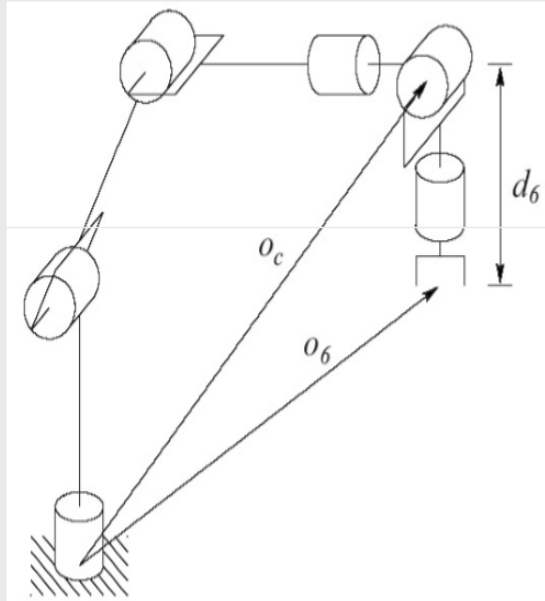
$$R_6^0(q_1, q_2, \dots, q_6) = R$$

$$o_6^0(q_1, q_2, \dots, q_6) = o$$

- Spherical wrist as paradigm.



- Let  $o_c$  be the intersection of the last 3 joint axes; as  $z_3$ ,  $z_4$ , and  $z_5$  intersect at  $o_c$ , the origins  $o_4$  and  $o_5$  will always be at  $o_c$ ; the motion of joints 4, 5 and 6 will not change the position of  $o_c$ ; only motions of joints 1, 2 and 3 can influence position of  $o_c$ .



$$o = o_c^0 + d_6 R \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

$$o = \begin{bmatrix} o_x \\ o_y \\ o_z \end{bmatrix} \quad o_c^0 = \begin{bmatrix} x_c \\ y_c \\ z_c \end{bmatrix}$$

$$\begin{bmatrix} x_c \\ y_c \\ z_c \end{bmatrix} = \begin{bmatrix} o_x - d_6 r_{13} \\ o_y - d_6 r_{23} \\ o_z - d_6 r_{33} \end{bmatrix} \Rightarrow q_1, q_2, q_3$$

$$R = R_3^0 R_6^3 \Rightarrow$$

$$R_6^3 = (R_3^0)^{-1} R = (R_3^0)^T R \Rightarrow q_4, q_5, q_6$$